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Specification and Drawing, as originally filed, with Application for Patent Serial No:
2,462,011, on February 23, 2004, by BAYER INC., assignee of Frederic Guerin, for
"Process for the Preparation of Low Molecular Weight Nitrile Rubber". PG 1162

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POS 1162 CA

IAP11 Rec'd PCT/PTO 17 AUG 2006**Abstract**

The present invention relates to a process for the production of, optionally hydrogenated, nitrile rubber polymers having lower molecular weights and narrower molecular weight distributions than those known in the art.

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POS 1162 CA

IAP11 Rec'd PCT/PTO 17 AUG 2006

Process for the Preparation of Low Molecular Weight Nitrile Rubber**Field of the Invention.**

The present invention relates to a process for the production of,
5 optionally hydrogenated, nitrile rubber polymers having lower molecular
weights and narrower molecular weight distributions than those known in the
art.

Background of the Invention

10 Hydrogenated nitrile rubber (HNBR), prepared by the selective
hydrogenation of acrylonitrile-butadiene rubber (nitrile rubber; NBR, a co-
polymer comprising at least one conjugated diene, at least one unsaturated
nitrile and optionally further comonomers), is a specialty rubber which has very
good heat resistance, excellent ozone and chemical resistance, and excellent
15 oil resistance. Coupled with the high level of mechanical properties of the
rubber (in particular the high resistance to abrasion) it is not surprising that
NBR and HNBR has found widespread use in the automotive (seals, hoses,
bearing pads) oil (stators, well head seals, valve plates), electrical (cable
sheathing), mechanical engineering (wheels, rollers) and shipbuilding (pipe
20 seals, couplings) industries, amongst others.

Commercially available NBR and HNBR have a Mooney viscosity in the
range of from 55 to 105, a molecular weight in the range of from 200,000 to
500,000 g/mol, and for the HNBR a polydispersity greater than 3.0 and a
residual double bond (RDB) content in the range of from 1 to 18% (by IR
25 spectroscopy).

One limitation in processing NBR and HNBR is the relatively high
Mooney viscosity. In principle, NBR and HNBR having a lower molecular
weight and lower Mooney viscosity would have better processability. Attempts
have been made to reduce the molecular weight of the polymer by mastication
30 (mechanical breakdown) and by chemical means (for example, using strong
acid), but such methods have the disadvantages that they result in the

1162 CA

introduction of functional groups (such as carboxylic acid and ester groups) into the polymer, and the altering of the microstructure of the polymer. This results in disadvantageous changes in the properties of the polymer. In addition, these types of approaches, by their very nature, produce polymers having a
5 broad molecular weight distribution.

A, optionally hydrogenated, nitrile rubber having a low Mooney (<55) and improved processability, but which has the same microstructure as those rubbers which are currently available, is difficult to manufacture using current technologies. The hydrogenation of NBR to produce HNBR results in an even
10 bigger increase in the Mooney viscosity of the raw polymer. This Mooney Increase Ratio (MIR) is generally around 2, depending upon the polymer grade, hydrogenation level and nature of the feedstock. Furthermore, limitations associated with the production of NBR itself dictate the low viscosity range for the HNBR feedstock. Currently, one of the lowest Mooney viscosity
15 products available is Therban® VP KA 8837 (available from Bayer), which has a Mooney viscosity of 55 (ML 1+4 @ 100°C) and a RDB of 18%.

Karl Ziegler's discovery of the high effectiveness of certain metal salts, in combination with main group alkylating agents, to promote olefin polymerization under mild conditions has had a significant impact on chemical
20 research and production to date. It was discovered early on that some "Ziegler-type" catalysts not only promote the proposed coordination-insertion mechanism but also effect an entirely different chemical process, that is the mutual exchange (or metathesis) reaction of alkenes according to a scheme as shown in Figure 1.

25 Acyclic diene metathesis (or ADMET) is catalyzed by a great variety of transition metal complexes as well as non-metallic systems. Heterogeneous catalyst systems based on metal oxides, sulfides or metal salts were originally used for the metathesis of olefins. However, the limited stability (especially towards hetero-substituents) and the lack of selectivity resulting from the
30 numerous active sites and side reactions are major drawbacks of the heterogeneous systems.

POS 1162 CA

Homogeneous systems have also been devised and used to effect olefin metathesis. These systems offer significant activity and control advantages over the heterogeneous catalyst systems. For example, certain Rhodium based complexes are effective catalysts for the metathesis of 5 electron-rich olefins.

The discovery that certain metal-alkylidene complexes are capable of catalyzing the metathesis of olefins triggered the development of a new generation of well-defined, highly active, single-site catalysts. Amongst these, Bis-(tricyclohexylphosphine)-benzylidene ruthenium dichloride (commonly 10 known as Grubb's catalyst) has been widely used, due to its remarkable insensitivity to air and moisture and high tolerance towards various functional groups. Unlike the molybdenum-based metathesis catalysts, this ruthenium carbene catalyst is stable to acids, alcohols, aldehydes and quaternary amine salts and can be used in a variety of solvents (C_6H_6 , CH_2Cl_2 , THF, $t\text{-BuOH}$).

15 The use of transition-metal catalyzed alkene metathesis has since enjoyed increasing attention as a synthetic method. The most commonly-used catalysts are based on Mo, W and Ru. Research efforts have been mainly focused on the synthesis of small molecules, but the application of olefin metathesis to polymer synthesis has allowed the preparation of new polymeric 20 material with unprecedented properties (such as highly stereoregular poly-norbornadiene).

25 The utilization of olefin metathesis as a means to produce low molecular weight compounds from unsaturated elastomers has received growing interest. The principle for the molecular weight reduction of unsaturated polymers is shown in Figure 2. The use of an appropriate catalyst allows the cross-metathesis of the unsaturation of the polymer with the co-olefin. The end result is the cleavage of the polymer chain at the unsaturation sites and the generation of polymer fragments having lower molecular weights. In addition, another effect of this process is the "homogenizing" of the polymer chain 30 lengths, resulting in a reduction of the polydispersity. From an application and processing stand point, a narrow molecular weight distribution of the raw

FDS 1162 CA

polymer results in improved physical properties of the vulcanized rubber, whilst the lower molecular weight provides good processing behavior.

The so-called "depolymerization" of copolymers of 1,3-butadiene with a variety of co-monomers (styrene, propene, divinylbenzene and 5 ethylvinylbenzene, acrylonitrile, vinyltrimethylsilane and divinyldimethylsilane) in the presence of classical Mo and W catalyst system has been investigated. Similarly, the degradation of a nitrile rubber using WCl_6 and $SnMe_4$ or $PhC\equiv CH$ 10 co-catalyst was reported in 1988. However, the focus of such research was to produce only low molecular fragments which could be characterized by conventional chemical means and contains no teaching with respect to the preparation of low molecular weight nitrile rubber polymers. Furthermore, such processes are non-controlled and produce a wide range of products.

The catalytic depolymerization of 1,4-polybutadiene in the presence of substituted olefins or ethylene (as chain transfer agents) in the presence of 15 well-defined Grubb's or Schrock's catalysts is also possible. The use of Molybdenum or Tungsten compounds of the general structural formula $\{M(=NR_1)(OR_2)_2(=CHR)\}$; M = Mo, W to produce low molecular weight polymers or oligomers from gelled polymers containing internal unsaturation along the polymer backbone was claimed in US 5,446,102. Again, however, 20 the process disclosed is non-controlled, and there is no teaching with respect to the preparation of low molecular weight nitrile rubber polymers.

International Applications PCT/CA02/00966, PCT/CA02/00965, and WO-03/002613-A1 disclose that hydrogenated and non-hydrogenated nitrile rubber having lower molecular weights and narrower molecular weight 25 distributions than those known in the art can be prepared by the olefin metathesis of nitrile butadiene rubber, optionally followed by hydrogenation of the resulting metathesised NBR. These documents use so called Grubb's catalysts' that are different from the catalysts of the present invention.

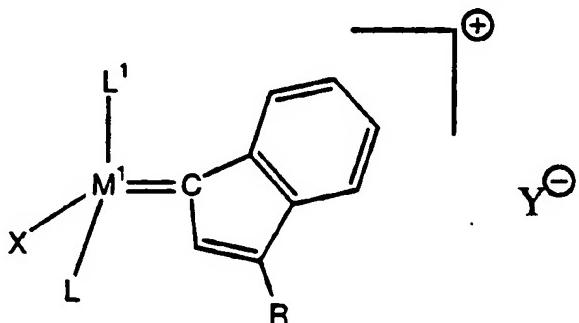
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Summary of the Invention

We have now discovered that, optionally hydrogenated, nitrile rubber having lower molecular weights and narrower molecular weight distributions than those known in the art can be prepared by the olefin metathesis of nitrile 5 butadiene rubber, in case of HNBR followed by hydrogenation of the resulting metathesised NBR.

Thus, one aspect of the disclosed invention is a process for the preparation of an, optionally hydrogenated, nitrile rubber comprising the steps of

- 10 a) reacting a nitrile rubber in the presence of at least one compound selected from the group consisting of compounds of the general formula I.



Formula 1

wherein:

- 15 M¹ is Os or Ru;

R is hydrogen or a hydrocarbon selected from the group consisting of C₂-C₂₀ alkenyl, C₂-C₂₀ alkynyl, C₁-C₂₀ alkyl, aryl, C₁-C₂₀ carboxylate, C₁-C₂₀ alkoxy, C₂-C₂₀ alkenyloxy, C₂-C₂₀ alkynyloxy, aryloxy, C₂-C₂₀ alcoxycarbonyl, C₁-C₂₀ alkylthio, C₁-C₂₀ alkylsulfonyl and C₁-C₂₀ alkylsulfinyl;

- 20 X is selected from any anionic ligand; and

L¹ is a neutral π-bonded ligand, preferably but not limited to arene, substituted arene, heteroarene, independent of whether they are mono- or polycyclic;

- 25 L is a ligand selected from the group consisting of phosphines, sulfonated phosphines, fluorinated phosphines, functionalized phosphines

POS 1162 CA

bearing up to three aminoalkyl-, ammoniumalkyl-, alkoxyalkyl-, alkoxy carbonylalkyl-, hydrocycarbonylalkyl-, hydroxylalkyl- or ketoalkyl- groups, phosphites, phosphinites, phosphonites, phosphinamines, arsines, stibenes, ethers, amines, amides, imines, sulfoxides, thioethers and pyridines;

- 5 Y is a non-coordinating anion; and optionally at least one co-olefin
and b) hydrogenation of the product of step a) if a hydrogenated nitrile rubber
is desired.

- The inventive process is capable of producing a hydrogenated nitrile
rubber having a molecular weight (M_w) in the range of from 30,000 to 250,000,
10 a Mooney viscosity (ML 1+4 @ 100 deg. C) of in the range of from 3 to 50, and
a MWD (or polydispersity index) of less than 2.5.

Brief Description of the Drawings

- Figure 1 shows a scheme of the mutual exchange (or metathesis)
15 reaction of alkenes.

- Figure 2 shows the principle for the molecular weight reduction of
unsaturated polymers.

Description of the Invention

- 20 As used throughout this specification, the term "nitrile polymer" (NBR) is
intended to have a broad meaning and is meant to encompass a copolymer
having repeating units derived from at least one conjugated diene, at least one
 α,β -unsaturated nitrile and optionally further one or more copolymerizable
monomers.

- 25 The conjugated diene may be any known conjugated diene, in
particular a C₄-C₆ conjugated diene. Preferred conjugated dienes are
butadiene, isoprene, piperylene, 2,3-dimethyl butadiene and mixtures thereof.
Even more preferred C₄-C₆ conjugated dienes are butadiene, isoprene and
mixtures thereof. The most preferred C₄-C₆ conjugated diene is butadiene.

- 30 The unsaturated α,β -unsaturated nitrile may be any known α,β -
unsaturated nitrile, in particular a C₃-C₅ α,β -unsaturated nitrile. Preferred C₃-C₅

α,β -unsaturated nitriles are acrylonitrile, methacrylonitrile, ethacrylonitrile and mixtures thereof. The most preferred C₃-C₅ α,β -unsaturated nitrile is acrylonitrile.

- Preferably, the copolymer comprises in the range of from 40 to 85 weight percent of repeating units derived from one or more conjugated dienes and in the range of from 15 to 60 weight percent of repeating units derived from one or more unsaturated nitriles. More preferably, the copolymer comprises in the range of from 60 to 75 weight percent of repeating units derived from one or more conjugated dienes and in the range of from 25 to 40 weight percent of repeating units derived from one or more unsaturated nitriles. Most preferably, the copolymer comprises in the range of from 60 to 70 weight percent of repeating units derived from one or more conjugated dienes and in the range of from 30 to 40 weight percent of repeating units derived from one or more unsaturated nitriles.
- 15 Optionally, the copolymer may further comprise repeating units derived from one or more copolymerizable monomers, such as unsaturated carboxylic acids. Non-limiting examples of suitable unsaturated carboxylic acids are fumaric acid, maleic acid, acrylic acid, methacrylic acid and mixtures thereof. Repeating units derived from one or more copolymerizable monomers will 20 replace either the nitrile or the diene portion of the nitrile rubber and it will be apparent to the skilled in the art that the above mentioned figures will have to be adjusted to result in 100 weight percent. In case of the mentioned unsaturated carboxylic acids, the nitrile rubber preferably comprises repeating units derived from one or more unsaturated carboxylic acids in the range of 25 from 1 to 10 weight percent of the rubber, with this amount displacing a corresponding amount of the conjugated diolefin.

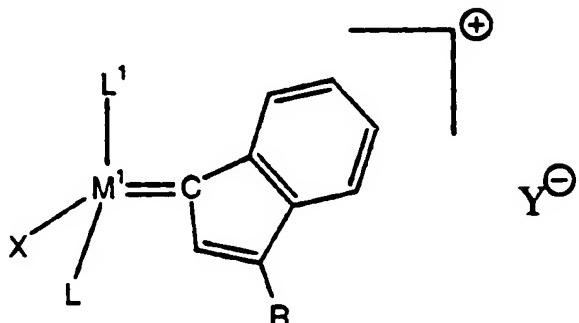
Other preferred optionally further monomers are unsaturated mono- or di-carboxylic acids or derivatives thereof (e.g., esters, amides and the like) including mixtures thereof.

- 30 To produce HNBR, the substrate is first subject to a metathesis reaction and then hydrogenated.

Metathesis

The metathesis reaction is conducted in the presence of one or more compounds of the general formula I

5



wherein:

M¹ is Os or Ru;

10 R is hydrogen or a hydrocarbon selected from the group consisting of C₂-C₂₀ alkenyl, C₂-C₂₀ alkynyl, C₁-C₂₀ alkyl, aryl, C₁-C₂₀ carboxylate, C₁-C₂₀ alkoxy, C₂-C₂₀ alkenyloxy, C₂-C₂₀ alkynyloxy, aryloxy, C₂-C₂₀ aloxycarbonyl, C₁-C₂₀ alkylthio, C₁-C₂₀ alkylsulfonyl and C₁-C₂₀ alkylsulfinyl;

X is selected from any anionic ligand; and

15 L¹ is a neutral π-bonded ligand, preferably but not limited to arene, substituted arene, heteroarene, independent of whether they are mono- or polycyclic;

L is a ligand selected from the group consisting of phosphines, sulfonated phosphines, fluorinated phosphines, functionalized phosphines 20 bearing up to three aminoalkyl-, ammoniumalkyl-, alkoxyalkyl-, alkoxycarbonylalkyl-, hydrocycarbonylalkyl-, hydroxyalkyl- or ketoalkyl- groups, phosphites, phosphinites, phosphonites, phosphinamines, arsines, stibenes, ethers, amines, amides, imines, sulfoxides, thioethers and pyridines;

Y is a non-coordinating anion;

POS 1162 CA

Compounds of Formula I wherein L is a trialkylphosphine, L¹ is 1-methyl-4-iso-propylphenyl, X is a chloride ion, R is phenyl and M is Ruthenium are preferred.

The amount of compounds will depend upon the nature and catalytic activity of the compound(s) in question. Typically, the ratio of compound(s) to NBR is in the range of from 0.005 to 5, preferably in the range of from 0.025 to 1 and, more preferably, in the range of from 0.1 to 0.5.

The metathesis reaction can be carried out in the absence of any co-olefin. However, the reaction rate is improved when the metathesis reaction is carried out in the presence of a co-olefin. The co-olefin may be a hydrocarbon or it may be functionalised, with the caveat that it should not inactivate the metathesis catalyst or otherwise interfere with the reaction. Preferred olefins include, but are not limited to, C₂ to C₁₆ linear or branched olefins such as ethylene, isobutene, styrene or 1-hexene. Where the co-olefin is a liquid (such as 1-hexene), the amount of co-olefin employed is preferably in the range of from 1 to 200 weight %. Where the co-olefin is a gas (such as ethylene) the amount of co-olefin employed is usually such that it results in a pressure in the reaction vessel in the range of from 2 * 10⁴ Pa to 2.5 * 10⁷ Pa, preferably in the range of from 1 * 10⁵ Pa to 1 * 10⁶ Pa and, more preferably, in the range of from 5.2 * 10⁵ Pa to 4 * 10⁶ Pa.

The metathesis reaction can be carried out in any suitable solvent which does not inactivate the catalyst or otherwise interfere with the reaction. Preferred solvents include, but are not limited to, dichloromethane, benzene, toluene, tetrahydrofuran, methyl ethyl ketone, cyclohexane and the like. The most preferred solvent is monochlorobenzene (MCB). In certain cases the co-olefin can itself act as a solvent (for example, 1-hexene), in which case no other solvent is necessary.

The concentration of NBR in the reaction mixture is not critical but, obviously, should be such that the reaction is not hampered if the mixture is too viscous to be stirred efficiently, for example. Preferably, the concentration of

US 1162 CA

NBR is in the range of from 1 to 40% by weight, most preferably in the range of from 6 to 15 wt.%.

The metathesis reaction is preferably carried out at a temperature in the range of from 20 to 140°C; more preferably in the range of from 60 to 120°C.

5 The reaction time will depend upon a number of factors, including cement concentration, amount of catalyst used and the temperature at which the reaction is performed. The metathesis is usually complete within the first two hours under typical conditions. The progress of the metathesis reaction may be monitored by standard analytical techniques, for example using GPC
10 or solution viscosity. Whenever referenced throughout the specification the molecular weight distribution of the polymer was determined by gel permeation chromatography (GPC) using a Waters 2690 Separation Module and a Waters 410 Differential Refractometer running Waters Millenium software version 3.05.01. Samples were dissolved in tetrahydrofuran (THF) stabilized with
15 0.025% BHT. The columns used for the determination were three sequential mixed-B gel columns from Polymer Labs. Reference Standards used were polystyrene standards from American Polymer Standards Corp.

Hydrogenation

20 Reduction of the product from the metathesis reaction can be effected using standard reduction techniques known in the art. For example, homogeneous hydrogenation catalysts known to those of skill in the art, such as Wilkinson's catalyst $\{(PPh_3)_3RhCl\}$ and the like can be used.

25 Processes for the hydrogenation of NBR are known and may also be used for the production of the hydrogenation products according to the invention. Rhodium or titanium is generally used as the catalyst, although platinum, iridium, palladium, rhenium, ruthenium, osmium, cobalt or copper in the form of the metals, but preferably in the form of metal compounds, may also be used, see for example US 3,700,637; DE-PS 2,539,132; EP-A-134
30 023; DE-OS 35 41 689; DE-OS 35 40 918; EP-A 298 386; DE-OS 35 29 252; DE-OS 34 33 392; US 4,464,515; and US 4,503,196.

Suitable catalysts and solvents for hydrogenation in homogeneous phase are described in the following, and in GB 1558491 of Bayer AG and in EP 471,250, previously incorporated herein by reference. It is not intended to restrict the catalysts and solvents for hydrogenation useful for the invention, 5 and these are provided only by way of example.

The selective hydrogenation can be achieved by means of a rhodium-containing catalyst. The preferred catalyst is of the formula



in which each R^8 is a C_1-C_8 -alkyl group, a C_4-C_8 -cycloalkyl group a C_6-C_{15} -aryl group or a C_7-C_{15} -aralkyl group, B is phosphorus, arsenic, sulfur, or a sulfoxide group $S=O$, X^3 is hydrogen or an anion, preferably a halide and more preferably a chloride or bromide ion, I is 2, 3 or 4, m is 2 or 3 and n is 1, 2 or 3, preferably 1 or 3. Preferred catalysts are tris-(triphenylphosphine)-rhodium(I)-chloride, tris(triphenylphosphine)-rhodium(III)-chloride and tris-10 (dimethylsulfoxide)-rhodium(III)-chloride, and tetrakis- (triphenylphosphine)-rhodium hydride of formula $((C_6H_5)_3P)_4RhH$, and the corresponding compounds in which triphenylphosphine moieties are replaced by tricyclohexyl-phosphine moieties. The catalyst can be used in small quantities. An amount in the range of 0.01 to 1.0% preferably 0.03% to 0.5%, most preferably 0.1% to 0.3% 15 by weight based on the weight of polymer is suitable.

It is known to use the catalyst with a co-catalyst that is a ligand of formula $R^8_m B$, where R, m and B are as defined above, and m is preferably 3. Preferably B is phosphorus, and the R groups can be the same or different. Thus there can be used a triaryl, trialkyl, tricycloalkyl, diaryl monoalkyl, dialkyl 25 monoaryl diaryl monocycloalkyl, dialkyl monocycloalkyl, dicycloalkyl monoaryl or dicycloalkyl monoaryl co-catalysts. Examples of co-catalyst ligands are given in US Patent No 4,631,315, the disclosure of which is incorporated by reference. The preferred co-catalyst ligand is triphenylphosphine. The co-catalyst ligand is preferably used in an amount in the range 0.3 to 5%, more

preferably 0.5 to 4% by weight, based on the weight of the copolymer. Preferably also the weight ratio of the rhodium-containing catalyst compound to co-catalyst is in the range 1:3 to 1:55, more preferably in the range 1:5 to 1:45. The weight of the co-catalyst, based on the weight of one hundred parts of 5 rubber, is suitably in the range 0.1 to 33, more suitably 0.5 to 20 and preferably 1 to 5, most preferably greater than 2 to less than 5.

The hydrogenation may be advantageously performed *in situ* i.e. in the same reaction vessel in which the metathesis step is carried out, without the need to first isolate the metathesised product. The hydrogenation catalyst is 10 simply added to the vessel, which is then treated with hydrogen to produce the HNBR.

Hydrogenation in this invention is understood by preferably more than 50 % of the residual double bonds (RDB) present in the starting nitrile polymer being hydrogenated, preferably more than 90 % of the RDB are hydrogenated, 15 more preferably more than 95 % of the RDB are hydrogenated and most preferably more than 99 % of the RDB are hydrogenated.

The low Mooney NBR and the preferred HNBR of the invention can be characterized by standard techniques known in the art. For example, the molecular weight distribution of the polymer was determined by gel permeation 20 chromatography (GPC) using a Waters 2690 Separation Module and a Waters 410 Differential Refractometer running Waters Millenium software version 3.05.01. Samples were dissolved in tetrahydrofuran (THF) stabilised with 0.025% BHT. The columns used for the determination were three sequential mixed-B gel columns from Polymer Labs. Reference Standards used were 25 polystyrene standards from American Polymer Standards Corp.

The Mooney viscosity of the rubber was determined using ASTM test D1646.

US 1162 CA

Examples**Examples 1-3**

Tris(triphenylphosphine)Rhodium Chloride (Wilkinson's
 5 hydrogenation catalyst), triphenylphosphine (TPP) and monochlorobenzene (MCB) were purchased from JMI, Elf Atochem and PPG respectively and used as received. The triflate (SO_3CF_3) salt of the cationic Tricyclohexylphosphine-(η^6 -1-methyl-4-iso-propylphenyl)-2-phenyl-indenylidene-Ruthenium chloride (Ru catalyst) was prepared as described in *Angew. Chem. Int. Ed. Engl.*; 2003,
 10 42, 4524-4527.

Metathesis

The metathesis reactions were carried out in a Parr high-pressure reactor under the following conditions:

15	Cement Concentration	12 wt.%
	Co-Olefin	Ethylene @ 400 psi
	Agitator Speed	600 rpm
	Reactor Temperature	80°C
	Ru Catalyst Loading	see Table A
20	Solvent	Monochlorobenzene
	Substrate	statistical Butadiene-acrylonitrile copolymer with an acrylonitrile content of 34 mol% and a Mooney-Viscosity ML (1+4)@ 100 deg. C of 35
25		

For example 1-2, the reactor was heated to desired temperature and 60mL of a monochlorobenzene solution containing the Rucatalyst was added to the reactor. The reactor was pressurised to the desired ethylene pressure.. The temperature was maintained constant for the duration of the reaction. A
 30 cooling coil connected to a temperature controller and a thermal sensor was

FDS 1162 CA

used to regulate the temperature. The progress of the reaction was monitored using solution viscosity measurements for the 6% cements.

Hydrogenation

The hydrogenation reactions were carried out in the same reactor as the metathesis under the following conditions:

	Cement solid concentration	12%
	H ₂ (g) pressure	1200 psi
	Agitator Speed	600 rpm
	Reactor Temperature	138°C
10	Catalyst Loading (Wilkinson's)	0.07 phr
	Triphenylphosphine	1 phr
	Solvent	Monochlorobenzene

The cement from the metathesis reaction was degassed 3 times with H₂ (100 psi) under full agitation. The temperature of the reactor was raised to 130°C and a 60mL monochlorobenzene solution containing Wilkinson's catalyst and triphenylphosphine was added to the reactor. The temperature was allowed to increase to 138°C and maintained constant for the duration of the reaction. The hydrogenation reaction was monitored by measuring the residual double bond (RDB) level at various intervals using IR spectroscopy.

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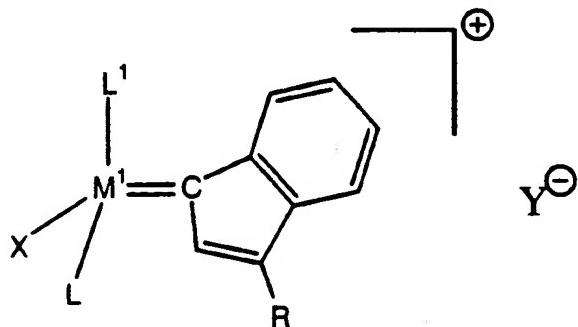
Table A Experimental Details

	Ex. 1	Ex.2	Therban® A3407 (Comparative)
Ru Catalyst Loading (phr)	0.035	0.016	N/A
Temperature	40°C	40°C	N/A
Ethylene Pressure	400 psi	400 psi	N/A
Final Residual Double Bond	< 1%	< 1%	<1%
Final Polymer Mooney (ML 1+4 @ 100°C)	28.2	43.9	65
GPC			
Mn (kg/mol)	64	83	97
Mw (kg/mol)	150	237	314
PDI	2.3	2.9	3.2

Therban® A3407 is available commercially from Bayer and is used for comparative purposes. It is produced using the same substrate as for example by simple hydrogenation. For a typical commercial product the Mn is 57kg/mol whilst the Mw is 314kg/mol. As expected, the molecular weight (Mw and Mn) are reduced by the metathesis reaction and the polymer weight distribution falls from 3.4 for the starting substrate to 2.0 for the metathesized product.

Claims

1. A process for the preparation of an, optionally hydrogenated, nitrile rubber comprising the steps of
 5 a) reacting a nitrile rubber in the presence at least one compound selected from the group consisting of compounds of the general formula I,



Formula 1

10

wherein:

M¹ is Os or Ru;

15 R is hydrogen or a hydrocarbon selected from the group consisting of C₂-C₂₀ alkenyl, C₂-C₂₀ alkynyl, C₁-C₂₀ alkyl, aryl, C₁-C₂₀ carboxylate, C₁-C₂₀ alkoxy, C₂-C₂₀ alkenyloxy, C₂-C₂₀ alkynyoxy, aryloxy, C₂-C₂₀ alkoxycarbonyl, C₁-C₂₀ alkylthio, C₁-C₂₀ alkylsulfonyl and C₁-C₂₀ alkylsulfinyl;

20 X is selected from any anionic ligand; and

L¹ is a neutral π -bonded ligand, preferably but not limited to arene, substituted arene, heteroarene, independent of whether they are mono- or polycyclic;

25 L is a ligand selected from the group consisting of phosphines, sulfonated phosphines, fluorinated

FDS 1162 CA

phosphines, functionalized phosphines bearing up to three aminoalkyl-, ammoniumalkyl-, alkoxyalkyl-, alkoxycarbonylalkyl-, hydrocycarbonylalkyl-, hydroxyalkyl- or ketoalkyl- groups, phosphites, phosphinites, phosphonites, phosphinamines, arsines, stibenes, ethers, amines, amides, imines, sulfoxides, thioethers and pyridines;

5

Y is a non-coordinating anion; and optionally further in the presence of at least one co-olefin and

10

and for the hydrogenated nitrile polymer

b) hydrogenating the product of step a).

- 15 2. A process according to claim 1 wherein the nitrile rubber is hydrogenated and the hydrogenation is performed under homogeneous catalytic conditions.
- 20 3. A process according to claim 2 wherein the hydrogenation is carried out *in situ*; that is, without first isolating the product of step a).
4. A process according to any of claims 1-3 wherein L is a trialkylphosphine, L¹ is 1-methyl-4-iso-propylphenyl, X is a chloride ion, R is phenyl and M is ruthenium.
- 25 5. A process according to any of claims 1-4 wherein the ratio of compound to nitrile rubber is in the range of from 0.005 to 5.
- 30 6. A process according to any of claims 1-5 when conducted in the presence of at least one co-olefin.

POS 1162 CA

7. A process according to any of claims claim 1-6 wherein the process is carried out in an inert solvent selected from the group consisting of monochlorobenzene, dichloromethane, benzene, toluene, tetrahydrofuran and cyclohexane.

5

8. A process according to any of claims 1-7 wherein the nitrile rubber is hydrogenated and the hydrogenation is carried out using a catalyst of formula :



10 wherein each R^8 is independently selected from the group consisting of a C₁-C₈-alkyl group, a C₄-C₈-cycloalkyl group, a C₆-C₁₅-aryl group and a C₇-C₁₅-aralkyl group;

B is selected from the group consisting of phosphorus, arsenic, sulfur, and a sulfoxide group (S=O) ;

15 X³ is selected from the group consisting of hydrogen and an anion; and

I is 2, 3 or 4, m is 2 or 3 and n is 1, 2 or 3.

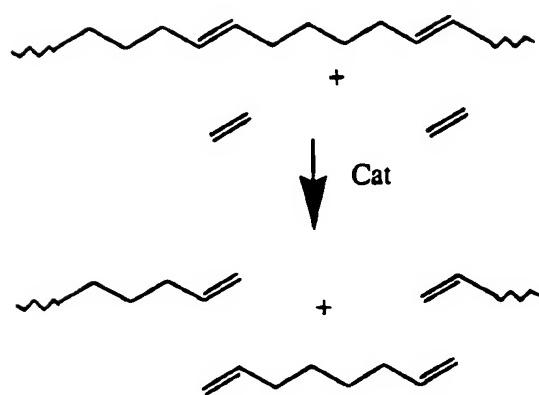
9. A process according to claim 8 wherein the hydrogenation catalyst is

20 (PPh₃)₃RhCl.

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**Figure 1**

5

**Figure 2**